2.2 kW Single-Mode Narrow-Linewidth Laser Delivery **Through a Hollow-Core Fiber**

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Antiresonant hollow-core fibers (AR-HCFs) have opened up exciting possibilities for high-energy and high-power laser delivery, thanks to their exceptionally low nonlinearities and high damage thresholds. While these fiber designs offer great potential for handling kilowatt-class powers, it is crucial to understand their fundamental limitations by investigating their performance at multi-kW power levels. Until now, efforts to deliver a narrow-linewidth single-mode laser at multi-kW power levels through a hollow core fiber have been unsuccessful. Here, we demonstrate the successful delivery of a record 2.2 kW laser power with a spectral linewidth of 84 GHz, centered at 1080 nm, while maintaining over 95% efficiency. This was achieved using a 6.25 m long AR-HCF with low-loss properties. Furthermore, we show power delivery of 1.7 kW with a spectral linewidth as narrow as 38 GHz. Our results could lead to a new generation of fiber-based laser beam delivery systems with applications in precision machining, nonlinear science, and directed energy.

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In recent years, the delivery of high-power single-mode laser beams through hollow-core optical fibers has undergone sub-2 stantial experimental advancements. These developments have 3 been fueled by the potential application of this technology in key areas including precision manufacturing [1], ultrafast physics [2–5], telecommunications [6–9], and directed energy [10–12] to 6 mention a few. In general, the goal of single-mode laser beam delivery fibers is to preserve the spectral and spatial features 8 of the source at a remote point of interest. This is especially 9 relevant in applications where beam focusing near the diffrac-10 tion limit is required to achieve high precision and accuracy. 35 11 Nevertheless, high-power transmission through solid core fibers 12 at long lengths suffer from numerous deleterious phenomena 13 due to intensity based non-linear effects such as the Kerr effect, 14 stimulated Raman scattering (SRS), and stimulated Brillouin 15 scattering (SBS) [13–15]. These effects impose significant con-16 straints on the power levels that can be transmitted through 17 a solid core optical fiber. In particular, high-power Ytterbium-18 doped (Yb-doped) single-mode narrow-linewidth fiber lasers 19 are typically restricted by SBS, while SRS limits high-power 20 broadband performance [10, 14]. 21

The concept of photonic bandgap introduced the possibil-22 ity of guiding light within an air-core confined by a precisely 23 engineered silica glass-air cladding structure [16]. Since then, 24

hollow core fibers have been extensively investigated leading to tremendous performance improvements and the demonstration of attenuation levels comparable to standard single-mode fibers [6, 9, 17–24]. In this regard, the emergence of antiresonant hollow core fibers (AR-HCF) offered unprecedented versatility in terms of tailoring the fiber modal properties and great promise for ultra-low loss light guidance [8, 9, 22–27]. In general, these structures consist of a negative curvature air-core interface, and rely on antiresonant and inhibited coupling as the light guiding mechanism [24, 28–33]. Various AR-HCF structures have been demonstrated, ranging from single resonator rings [18] and conjoined tubes [22] to nested [25] and double nested [8] configurations, spanning from strictly single-mode to multimode designs [19].

A unique feature of hollow core fibers is that light can be guided with a minimal fraction of the field overlapping with the glass structure, increasing the damage threshold and reducing material absorption and nonlinearity. Over the years, there have been numerous efforts on power transmission though hollow core fibers, including photonic bandgap [34] and hypocycloidalcore Kagome type structures [35] with single-mode laser power transmission experiments reaching up to 1.2 kW through 1.5 m of fiber [36]. Recent AR-HCF designs have shown great promise for scaling to extreme high-power single-mode delivery, due to

their strong confinement and large core diameter characteristics. 49 As such, the interest in exploring high-power delivery through 50 AR-HCFs has greatly intensified since the demonstration of 300 51 W single-mode broadband laser transport at 1 μ m through a 52 7-tube AR-HCF [37]. At the \sim 1000 W level, there have been 53 54 a few transmission demonstrations involving broad-linewidth 55 sources through both nested and non-nested AR-HCF designs [27, 38, 39]. Significantly, a recent study by Mulvad et al. [27] 56 successfully delivered 1.1 kW output power over across 1 km 57 of nested antiresonant nodeless fiber (NANF) using a 1080 nm 58 source with a spectral linewidth of approximately 6 nm. How-59 ever, despite these significant advancements, the transmission 60 of multi-kW powers or high-power narrow-linewidth sources 61 in a single-mode fashion remains out of reach. Additionally, 62 these investigations have highlighted the challenge of main-63 taining adequate coupling efficiency and preventing failure at 64 the fiber input, requiring optical alignment adjustments during 65 high-power operation. 66

In this work, we demonstrate transmission of multi-kW 67 narrow-linewidth single-mode power through a 6.25 m long 68 5-tube NANF. By coupling a 2.3 kW single-mode CW laser oper-69 ating at 1080 nm, with a beam quality (M^2) of 1.045, we achieved 70 an output power of 2.2 kW at 84 GHz linewidth, while maintain-71 ing near diffraction-limited beam quality. We precisely tailor the 72 beam coupled into the hollow core fiber, ensuring exceptional 73 stability and eliminating the need for realignment at high power 100 74 levels. Furthermore, for laser configurations with linewidths of 101 75 64 GHz and 38 GHz, we obtained output powers of 2.17 kW and 102 76 77 1.7 kW, respectively, limited only by the maximum power of the 103 source 78

The low-loss NANF used in the experiments was fabricated 105 79 in-house with attenuation of 0.79 dB/km at 1080 nm. In Fig. 106 80 107 1(a), we present a scanning electron microscope (SEM) image of 81 108 the NANF facet with core diameter of $\sim 23 \ \mu m$ and thickness of 82 outer tubes and nested tubes of 780 $nm \pm 10$ nm. The attenuation ¹⁰⁹ 83 spectrum was obtained via a 463 m cutback measurement, Fig. ¹¹⁰ 84 1(b). Using the $1/e^2$ definition, the mode field diameter (MFD) ¹¹¹ 85 was found to be ${\sim}18~\mu{\rm m}$ at 1080 nm, which is in excellent agree- 112 86 ment with the calculated MFD when simulating the structure ¹¹³ 87 114 shown in Fig. 1(a). 88 115

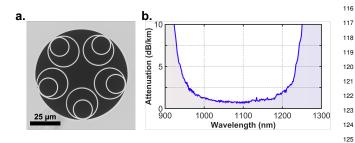


Fig. 1. Characterization of the fabricated NANF fiber. (a) SEM image of the 5-nested tubes NANF. (b) Measured spectral attenuation.

To investigate the power delivery performance of the NANF, 130 89 we employed a CW fiber laser amplifier system capable of pro- 131 90 ducing up to 2325 W with an 84 GHz linewidth. The laser source 91 132 utilized a three-stage Yb-doped fiber amplifier architecture and 133 92 an external seed connected to a phase modulator for spectral 134 93 broadening. The seed operated at a wavelength of 1080.14 nm 135 94 and a 1 MHz linewidth. Inline RF attenuators served to control 136 95 the resulting linewidth of the modulated seed. Figure 2, shows 137 96

a schematic of the experimental setup.

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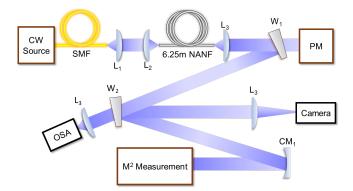


Fig. 2. Schematic of the experimental setup. A high-power CW fiber laser amplifier system is coupled into a 6.25 m long NANF. Large mode area (LMA) fiber; L₁, L₂, L₃, L₄, L₅ planoconvex lenses; W₁ and W₂ fused silica wedges; Power meter (PM); optical spectrum analyzer (OSA); M₁ plano-concave mirror.

The fiber laser output was delivered through a large mode area (LMA) fiber and collimated using a plano-convex lens (L_1). The resulting collimated beam was then free-space coupled to the 5-tube NANF which had a total length of 6.25 m. To match the mode field diameter of the NANF, a second plano-convex lens (L2) was used, resulting in a numerically calculated coupling efficiency of ~98%. To minimize localized thermal drift and distortion during operation, the fiber was mounted on a custom fixture, and precise alignment between the LMA fiber and the NANF was achieved using 5-axes stages. The NANF was coiled on an uncooled 25 cm diameter grooved aluminum mandrel. For power measurement and monitoring, the output of the NANF was collimated using the same method as the input and directed through an antireflection coated fused-silica wedge (W_1) . A low-power reflection from the wedge was fed into the beam diagnostics equipment. Over 99.93% of the fiber output power was captured and measured using a 5 kW power meter (Ophir 5000W-BB-50).

The output beam was characterized by conducting M², spectral, and mode profile measurements. To accomplish this, we utilized the first reflection of the low-power pickoff (W_1) , which was directed towards an uncoated fused-silica wedge (W2). The transmitted light through W₂ was then coupled to an optical spectrum analyzer (OSA) with a resolution of 7.5 GHz (Thorlabs BP209-IR2) using a single-mode fiber patch cable. Simultaneously, the front surface reflection from W2 was directed towards a beam profiler to determine the beam divergence and calculate the M² values in the X and Y directions. For imaging purposes, the back surface reflection of W₂ was captured by a CMOS camera through a 400 mm focal length lens (L₅) providing adequate magnification. It is important to note that in our experimental setup, the imaged beam originates from back reflections of W_2 , resulting in the beam passing through the wedge material twice. This introduces a slight elliptical distortion at the image plane due to the wedge.

Coupling from the laser LMA fiber to the NANF was performed at low power (below 5W). At this point, we measured a transmission efficiency of 97.3% through the NANF. After we optimized the input coupling conditions at low power, no additional adjustments to the NANF input coupling were performed

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for the entire duration of high power testing. Subsequently, we 138 increased the power to about 20 W. This higher power allowed 139 us to align the optical diagnostics components, as illustrated in 153 140 Fig. 2. After diagnostics alignment at this power level, we grad-141 ually increasing the power in \sim 220W increments. At each power 155 142 increment, we allocated a 120-second pause to monitor any po- 156 143 tential thermal drift and to ensure that the power meter reached 157 144 a steady state before recording measurements. The temperature 158 145 of the fiber was continuously monitored using a handheld ther- 159 146 mal camera (FLIR T560). The first evaluation at high power was 160 147 conducted with an 84 GHz linewidth and subsequently repeated 161 148 at 64 GHz and 38 GHz linewidths. 149

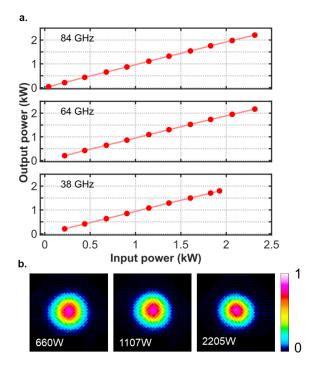


Fig. 3. Experimental narrow-linewidth laser delivery through hollow core fiber. (a) Output power as function of input power for three different source linewidth configurations. (b) Far field beam profiles at the output of the 6.25 m NANF for different transmitted powers at 84 GHz linewidth.

Input	Input	Output	Transmission
Power (W)	\mathbf{M}^2	\mathbf{M}^2	Efficiency
$\pm 4\%$	$\pm 5\%$	$\pm 5\%$	$\pm 0.5\%$
219	1.065	1.050	96.4%
678	1.050	1.035	96.8%
1147	1.045	1.035	96.7%
1605	1.045	1.030	96.0%
2066	1.045	1.015	95.9%
2315	1.045	1.020	95.3%

Table 1. Beam quality and transmission efficiency measurements with the single-mode 84 GHz linewidth source

In Fig. 3(a), we present the power transmission results for the 184 150

three different spectral linewidth conditions. Beam profiles corresponding to 0.5 kW, 1 kW, and 2kW transmission outputs are depicted in Fig. 3(b). The maximum laser power of the source was limited to 2.315 kW for both 84 GHz and 64 GHz, and further limited to 1.828 kW at 38 GHz. Our experimental findings demonstrate successful laser delivery through the NANF, with power values of 2.205 kW, 2.170 kW, and 1.708 kW achieved at 84 GHz, 64 GHz, and 38 GHz, respectively. At maximum power, these results correspond to transmission efficiencies of 95.4%, 94%, and 93.6% for each respective linewidth. The slightly lower efficiencies observed for the latter two cases can be attributed to micrometer scale misalignment of the coupling conditions. The fiber input launching conditions were not re-optimized during the experiments, which emphasizes the stability of the NANF and input coupling optics.

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166 Throughout the study, the temperature at the input interface of the NANF remained below 82°C, while the temperature along 167 the length of the fiber did not exceed 42°C. We collected beam 168 quality measurements at each input power step, and the results 169 for the 84 GHz linewidth case are shown in Table 1, alongside 170 the corresponding transmission efficiency. M² is reported as the 171 total M² defined as $M^2 = \sqrt{M_x^2 M_y^2}$. We observed a slight decrease 172 in transmission efficiency as the input power was increased, 173 as can be seen in Table 1. This could be attributed to minor 174 alignment drift at the NANF input or slight beam distortions 175 caused by thermal lensing on the coupling optics. 176

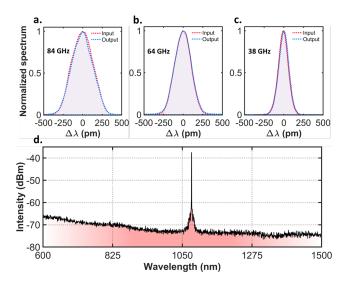


Fig. 4. Spectral characterization of the laser beam. Spectral measurements obtained at maximum power for each source linewidth configuration: (a) 84 GHz, (b) 64 GHz, (c) 38 GHz. Measured input signal spectra from the laser source are depicted in red, while the NANF output spectra are represented in blue. (d) Measured output spectrum covering the spectral wavelength range from 600 nm to 1500 nm for 2.2 kW and 84 GHz transmission.

To gain a better understanding of potential nonlinear distortions in the NANF, we conducted spectral measurements at the maximum transmitted powers for each linewidth configuration, as depicted in Fig. 4. Narrow wavelength scans are shown in Figs. 4(a-c) corresponding to 84 GHz, 64 GHz, 38 GHz inputs, respectively. The central wavelength corresponds to 1080 nm. For each case, the measured input signal spectra from the fiber laser source are depicted in red, while the NANF output spectra

are represented in blue. One can observe that the linewidth of 247 185 the source is preserved through the fiber. In addition, we per- 248 186 formed a wavelength scan covering the spectral range from 600 249 187 250 nm to 1500 nm for 2.2 kW output power at 84 GHz as shown in 188 251 Fig. 4(d). Under these conditions, the spectrum exhibits only the 189 central peak of the source located near 1080 nm. These measure-190 253 ments confirm that there are no additional spectral features or 191 254 broadening attributed to nonlinear processes resulting from the 192 255 high energy densities within the NANF. 193 256

In conclusion, we have demonstrated delivery of narrow- 257 194 linewidth single-mode laser power through a hollow core fiber 258 195 at a record average power of 2.2 kW. This was enabled by an 259 196 in-house fabricated low-loss 5-tube NANF, which exhibits a loss 260 197 261 of 0.79 dB/km at 1080 nm. We have shown that our NANF can 198 262 reliably transmit high power levels, achieving output powers of 199 263 2.2 kW, 2.17 kW, and 1.7 kW, with spectral linewidths of 84 GHz, 200 264 64 GHz, and 38 GHz, respectively. The measured transmission 201 265 efficiency was above 95% at 2.2 kW. Furthermore, our fiber pro-202 266 vides robust single-mode performance with M² of 1.045. The 203 267 NANF effectively mitigates nonlinear effects, as evidenced by 204 268 the absence of measurable nonlinear distortions in the delivered 205 269 laser beam. Our results could pave the way for high-brightness 206 270 narrow-linewidth fiber delivery systems for a wide range of 271 207 applications. 272 208

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216 **Disclosures.** The authors declare no conflicts of interest.

217Data availability.Data underlying the results presented in this
paper are not publicly available at this time but may be obtained from
the authors upon reasonable request.284
285219the authors upon reasonable request.286

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